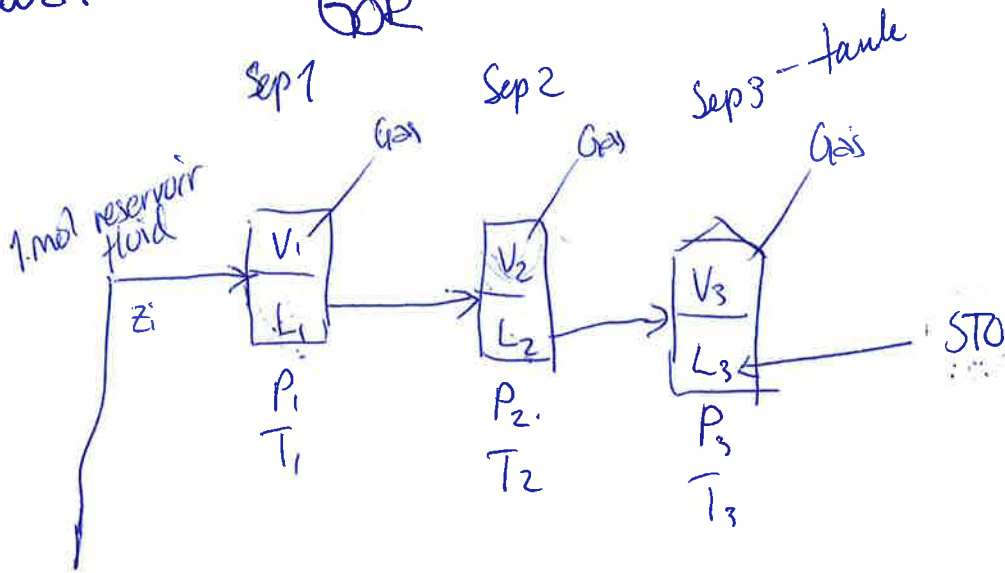


GOR



$$\text{GOR total} = \frac{V_{g, \text{sc}}}{V_{\text{STO}, \text{sc}}} = \frac{n_g \cdot V_m \cdot \rho_{\text{STO}}}{n_{\text{STO}} \cdot M_{\text{STO}}} = \frac{\left(1 - \prod_{i=1}^k L_i\right) \cdot V_m \cdot \rho_{\text{STO}}}{\prod_{i=1}^k L_i \cdot M_{\text{STO}}}$$

GOR for separator i : Based on 1 mol initial fluid

$$\text{GOR}_i = \frac{(V_g)_i}{V_{\text{STO}}} = \frac{(N_g)_i \cdot V_m \cdot \rho_{\text{STO}}}{n_{\text{STO}} \cdot M_{\text{STO}}} = \frac{V_i \cdot \prod_{j=1}^{i-1} L_j \cdot V_m \cdot \rho_{\text{STO}}}{\prod_{j=1}^k L_j \cdot M_{\text{STO}}}$$

$(N_g)_i$ = number of moles gas in sep i .

$$\text{GOR}_i = \frac{V_i \cdot V_m \cdot \rho_{\text{STO}}}{\prod_{j=1}^k L_j \cdot M_{\text{STO}}}$$

Example: We have k separators,
 k is stock tank

Find GOR for separator 4.

$$GOR_4 \quad i = 4$$

$$GOR_i = \frac{V_i - \left(\prod_{i=1}^{i-1} L_i \right) \cdot V_m \cdot \rho_{STO}}{\prod_{i=1}^k L_i \cdot M_{STO}}$$

$$GOR_4 = \frac{V_4 \cdot \cancel{L_1} \cdot \cancel{L_2} \cdot \cancel{L_3} \cdot V_m \cdot \rho_{STO}}{\cancel{L_1} \cdot \cancel{L_2} \cdot \cancel{L_3} \cdot L_4 \cdot L_5 \cdot \dots \cdot L_k \cdot M_{STO}}$$

$$GOR_4 = \frac{V_4 \cdot V_m \cdot \rho_{STO}}{\prod_{i=4}^k L_i \cdot M_{STO}}$$

$$GOR_{tot} = GOR_1 + GOR_2 + \dots + GOR_{tank}$$

④ Formation volume factor, B_o

B_o defined as the ratio between the reservoir volume of the oil and the stock tank volume of oil (at standard conditions)

If $P > P_b$, we have 1 mol reservoir oil (n_o), with molecular weight M_o

$$B_o = \frac{V_{\text{reservoir oil}} (V_o)}{V_{\text{stock tank oil}} (V_{STO})} = \frac{\overset{=1}{n_o} \cdot M_o}{\rho_o} = \frac{M_o \cdot \rho_{STO}}{\prod_{i=1}^k L_i \cdot M_{STO} \cdot \rho_o}$$

M_o = molar weight of reservoir oil

ρ_o = density of reservoir oil

M_{STO} = molar weight of STO

ρ_{STO} = density of STO

n_{STO} = number of moles STO

Units: m^3/Sm^3 , bbl/SBL

Example : Calculate GOR and Bo - factor

A reservoir oil produced through a 3-step separator system.

Flash equations and calculations, based on reservoir oil composition, z_i , corresponding K_i -values

Mole fractions of liquid and gas in every separation step.

$$\text{Sep 1 : } V_1 = 0.5061 \quad L_1 = 0.4939$$

$$\text{Sep 2 : } V_2 = 0.3145 \quad L_2 = 0.6855$$

$$\text{Sep 3 : } V_3 = 0.2222 \quad L_3 = 0.7778$$

Bo (single flash) - only one separation = $2.15 \text{ m}^3/\text{Sm}^3$

$$\rho_{\text{STO}} = 882 \text{ kg}/\text{Sm}^3$$

$$\rho_{\text{reservoir oil}} = 567.8 \text{ kg}/\text{m}^3$$

$$M_{\text{STO}} = 169.3 \text{ kg}/\text{kg mol}$$

$$M_o = 55.9 \text{ kg}/\text{kg mol}$$

$$V_m = 23.65 \text{ Sm}^3/\text{kg mol}$$

Start with 1 kgmol feed

$$\text{Total GOR}_t = \frac{V_g}{V_{\text{STO}}} = \frac{n_g \cdot V_m}{\frac{M_{\text{STO}}}{\rho_{\text{STO}}}} = \frac{n_g \cdot V_m}{\frac{M_{\text{STO}}}{\rho_{\text{STO}}}}$$

$$= \frac{(1 - \prod_{i=1}^k L_i) \cdot V_m \cdot \rho_{\text{STO}}}{\prod_{i=1}^k L_i \cdot M_{\text{STO}}} = \frac{(1 - L_1 \cdot L_2 \cdot L_3) \cdot V_m \cdot \rho_{\text{STO}}}{L_1 \cdot L_2 \cdot L_3 \cdot M_{\text{STO}}}$$

$$= \frac{(1 - 0.263) \cdot 23.65 \cdot 882 \frac{\text{kg}}{\text{Sm}^3}}{0.263 \text{ kg mol} \cdot 169.3 \text{ kg/kg mol}} = \underline{\underline{345,1 \frac{\text{Sm}^3}{\text{Sm}^3}}}$$

$$N_0 = 1 \text{ kg mol feed}$$

$$\underline{\underline{B_0}} = \frac{V_0}{V_{STO}} = \frac{\frac{m_0}{\rho_0}}{\frac{m_{STO}}{\rho_{STO}}} = \frac{\frac{N_0 \cdot M_0}{\rho_0}}{\frac{m_{STO} - M_{STO}}{\rho_{STO}}} = \frac{1 \text{ kg mol} \cdot 55.9 \frac{\text{kg}}{\text{kg mol}} \cdot 882 \frac{\text{kg}}{\text{Sm}^3}}{169.3 \frac{\text{kg}}{\text{kg mol}} \cdot 567.8 \frac{\text{kg}}{\text{m}^3} \cdot \prod_{i=1}^k L_i (0.263)}$$

$$= \frac{1 \text{ kg mol} \cdot M_0}{\dots}$$

$$= \underline{\underline{1.95 \frac{\text{m}^3}{\text{Sm}^3}}}$$

$$B_0(\text{sep}) < B_0(\text{single flash})$$

Lower B_0 means higher V_{STO}

\Rightarrow separation process is good!

EXAM AUTUMN 2012

PROBLEM NO. 1

Given reservoir and fluid data:

Bulk volume: 10^6 m^3

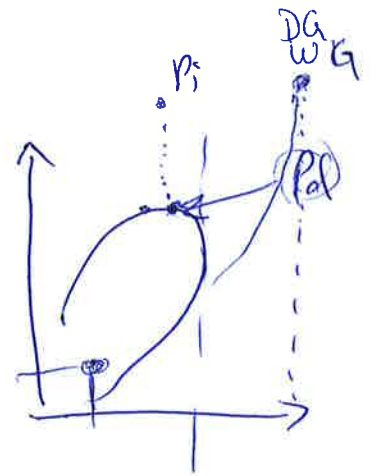
$\Phi = 0.23$

$S_{wi} = 0.15$

$P_i = 350 \text{ bar}$, $(Z_g)_i = 1.107$

$P_d = 201 \text{ bar}$

$T_{res} = 115^\circ \text{C}$



Data from CVD - analysis:

$V_{\text{cell}} = 950 \text{ cm}^3$ at P_d and T_{res}

Pres bar	ΔV cm^3	% of V_{cell}	Z_g
201	0	0	0.771
170	170	6.2	0.794
136	220	8.2	0.805
102	340	10.1	0.835
68	550	7.9	0.875
34	1000	7.1	0.945

Composition of well stream in mol %

Pres bar	C1	C2	C3	C4	C5	C6	C7+	
201	75.2	7.7	4.4	3.1	2.2	2.2	5.2	100 %
170	78.8	7.7	4.3	2.8	1.9	1.6	3.4	100 %

Separation conditions:

$C_1 - C_4$: became gas

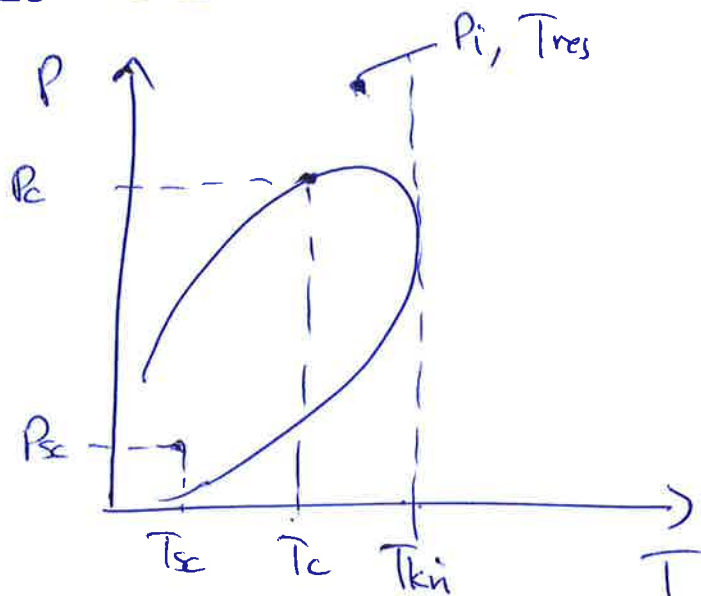
$C_5 - C_{7+}$: became STO

$$\rho_{STO} = 775 \text{ kg/m}^3 \quad M_{STO} = \text{143} \text{ kg/kg mol } P_i - P_d$$

$$\rho_{STO} = 750 \text{ kg/m}^3 \quad M_{STO} = 138 \text{ kg/kg mol } P_d = 170 \text{ bar}$$

a) 1. Characterize the reservoir fluid using \Rightarrow PT-diagram.

Gas condensate reservoir



$T_c < T_{res} < T_{ki}$
So inside
the two phase
area

2. CVD - analysis:

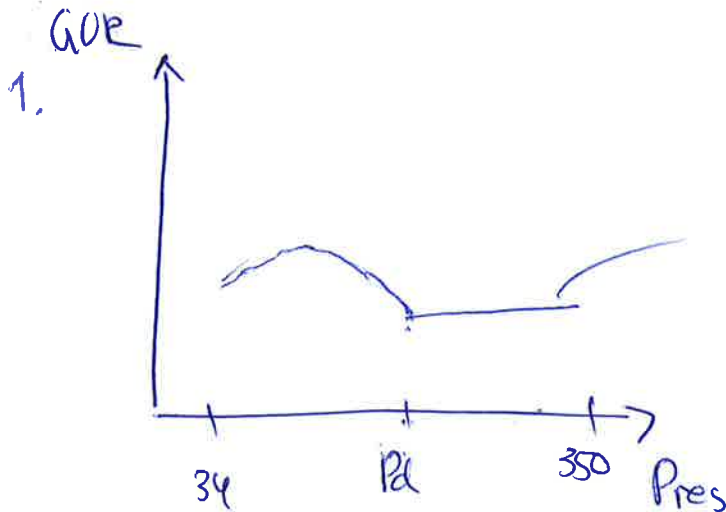
- Used to simulate behaviour of reservoir fluid in the reservoir ~~at~~ by depletion.
- Take separator gas and stock tank oil, recombined to same ~~as~~ composition as reservoir fluid at P_d, T_{res} , into a PVT-cell, at P_d and T_{res} . Volume at P_d, T_{res} is noted.

- Increase cell volume to decrease pressure
 $\Delta V_1, P_1$
- Gas volume ΔV_1 is produced, P_1 is held constant.
- Measure Z-factors
Composition of oil and gas
- Retrograde liquid volume condensed, V_L
- Reduce pressure again to P_2

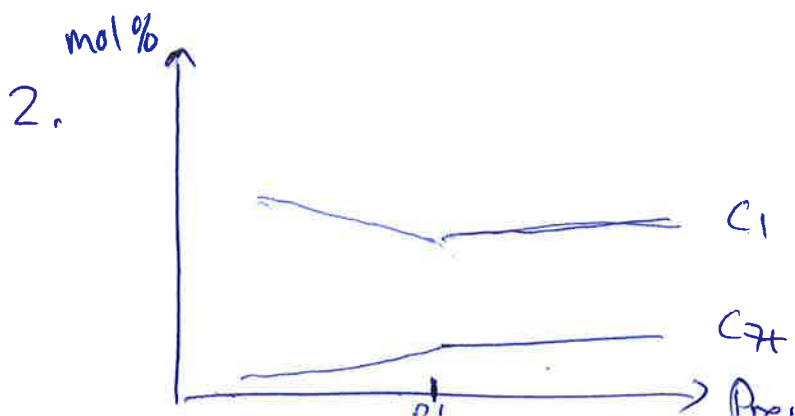


Continue until a certain pressure.

b) For $P_1: 34 < P_{res} < 350$ bar



constant GOR at $P_{res} > P_d$
reservoir fluid has
constant composition.



C_1
 C_{7+}

3. liquid volume

