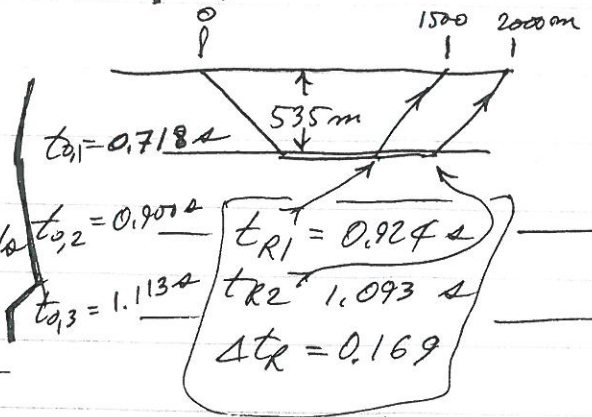


# BPG-150 Exam 2013-11-28

1.  $\alpha_1$ , vel. of seawater



3

(a)  $\alpha_1 = \frac{2h_1}{t_{0,1}} = \frac{1070}{0.718} = 1490 \text{ m/s}$   
 (1490.25)

3

(b) Refractions  $\nearrow$   $\alpha_2 = \frac{500}{0.169}$

$\alpha_2 = 2960 \text{ m/s}$  (2958.58)

(c)  $V_{s,3} = 2300 \text{ m/s}$

$\alpha_{2,3} = \left[ \frac{V_{s,3}^2 t_3 - V_{s,2}^2 t_2}{t_3 - t_2} \right]^{1/2}$

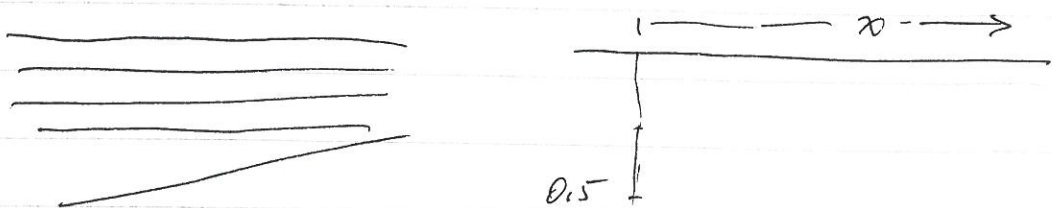
let  $V_{ens} = V_s$

We need to find  $V_{s,2} = \left[ \frac{\alpha_1^2 t_1 + \alpha_2^2 t_2}{t_1 + t_2} \right]^{1/2}$

$V_{s,2} = 1882 \text{ m/s}$  (1881.975)

$\alpha_3 = 3560.43 \text{ m/s}$  (3560.43)  $\alpha = 3560 \text{ m/s}$

4



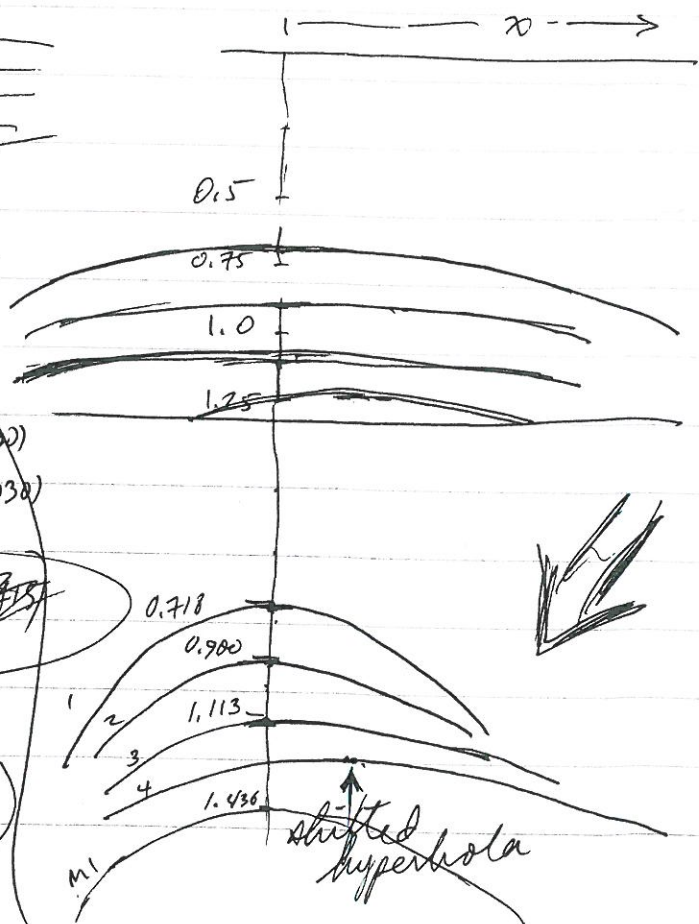
(e)  $R_{12} = \frac{\alpha_2 l_2 - \alpha_1 l_1}{\alpha_2 l_2 + \alpha_1 l_1}$

$R_{12} = \frac{310 \cdot \alpha_2^{574} - \alpha_1 \cdot (1000 - 1030)}{310 \cdot \alpha_2^{574} + \alpha_1 \cdot (1000 - 1030)}$

~~$R_{12} = \dots$~~

$= 0.630 - 0.639$

$R_{12} = 0.63 - 0.64$



$$0.168^2 + 2150^{-2} x^2 = 0.302^2 + 2710.18^{-2} x^2$$

$$x^2 \left( \frac{1}{2150^2} - \frac{1}{2710.18^2} \right) = 0.302^2 - 0.168^2$$

17 (8) 4 2 3  
 16 (6) b) 3 4  
 (5) c) 4

19  
 e) 4+3  
 b) 2  
 a) 2  
 b) 4  
 c) 3  
 d) 1/2

1/4  
 1/4  
 3/4  
 1/4  
 1/4  
 2+1/2

Taking as 23  
 + finding new V<sub>s,3</sub>  
 + inst. of ↑  
 in both

2958.58  
 $\rho_2 \approx 310 \cdot \alpha_2^{1/4}$   
 $= 2286.30 \text{ kg/m}^3$

$\rho_1 \approx 1025 \text{ kg/m}^3$

$\rho_1 = \rho_2$   
 -3 1/2

3 1/2 for 0.404  
 (too much Gardner)  
 4/5 1/2 for no Gardner  
 but rest.

1. (f)  $\frac{1}{\alpha_2} = \left[ \frac{\phi}{\alpha_w} + \frac{1-\phi}{\alpha_m} \right]$  or  $\frac{1-\phi}{\alpha_m} = \frac{1}{\alpha_2} - \frac{\phi}{\alpha_w}$

4

Then  $\alpha_m = (1-\phi) \left[ \frac{1}{\alpha_2} - \frac{\phi}{\alpha_w} \right]^{-1} = 0.8 \left[ \frac{-0.2}{1490.25} + \frac{1}{2958.58} \right]$

$\alpha_m = 3925.525$  or  $3926 \text{ m/s}$

$\frac{1}{2}/4$  if  $\alpha_2$  &  $V_m$  interchanged

2. (a)
1. Drift — to correct for 'drift': change in instrument reading w. time at same place
  2. Latitude — to correct for normal change of  $g$  with N-S displacement / latitude
  3. Free-air — to correct for normal change of  $g$  w. elevation above MSL or ref. elev'n
  4. Bouguer — to correct for effect of mass between ref. elev'n and reading elev'n
  5. Eötvös — to correct for effect of moving instrument on ship or other moving platform
  6. Terrain — for effect of very rugged terrain near obs. points
  - (7. Tidal — for Earth tides (deformation due to Sun's & Moon's gravity))

10

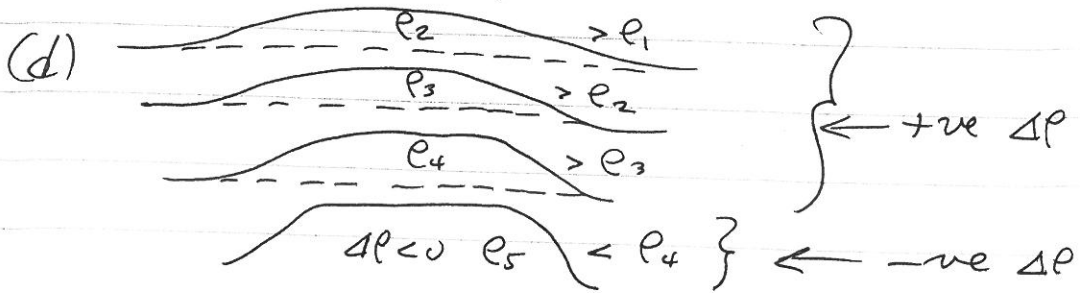
$4\frac{1}{2}$

- (b) At the poles  $\left[ \frac{1}{2} \times 3 \right]$
- least reduction of  $g$  from centripetal effect
  - closest to centre of mass / of Earth

3 1/2

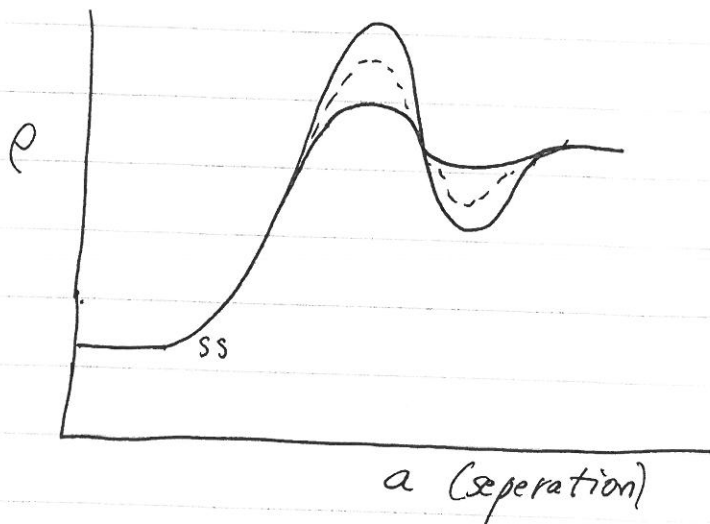
- (c) 1. Diurnal correction - to correct for change in mag. field during day due to Sun  
 2. Geomagnetic - to correct for normal (average) variation of field over Earth

3



4

- (e)
- 1 SS  $\phi$  high, brine high salinity  $\Rightarrow$  v. low  $\rho$
  - 2 salt  $\Rightarrow$  v. high  $\rho$
  - 3 SH  $\phi$  low, brine low salinity  $\Rightarrow$  low  $\rho$
  - 4 SS  $\phi$  low, oil  $\Rightarrow$  high  $\rho$



### 3. Integrated

~~2 1/2~~

(a) Salt dome

(b) (i) reflection - seismic amplitude or ground vel'y or

(ii) gravity - accel'n or g

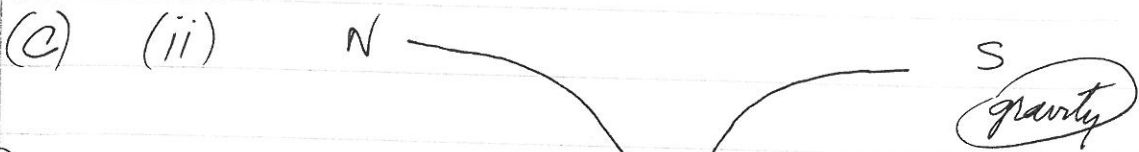
~~(iii) magnetic - field strength~~

~~(iii)~~ (iii) electrical - current density

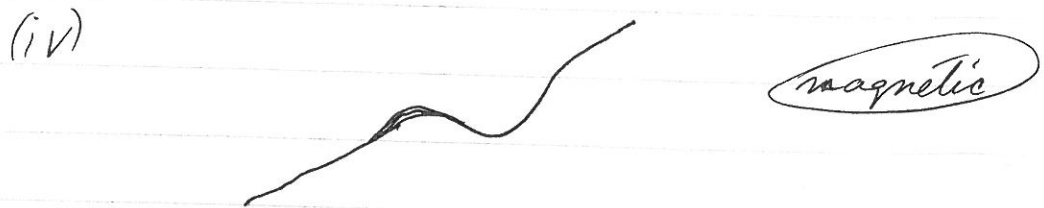
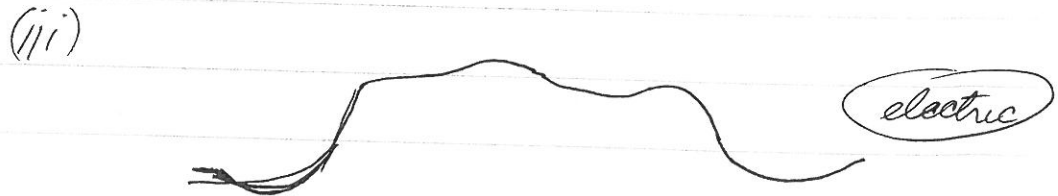
(iv) magnetic - field strength

(v) refraction/fan - ~~or~~ arrival times

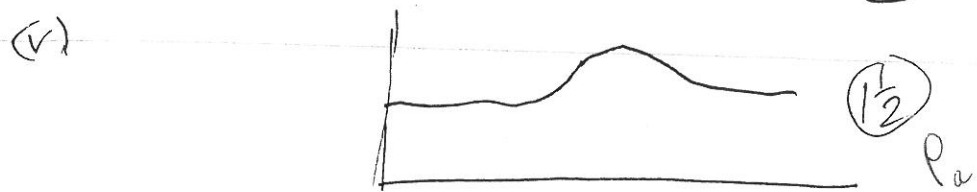
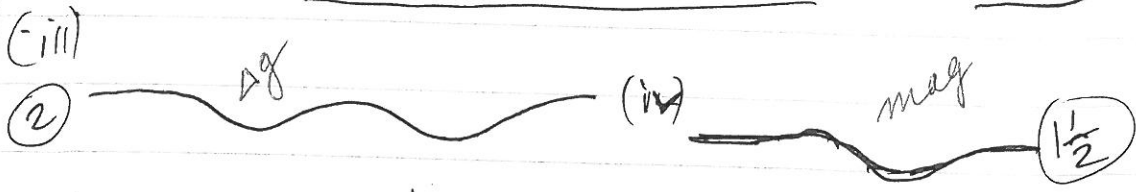
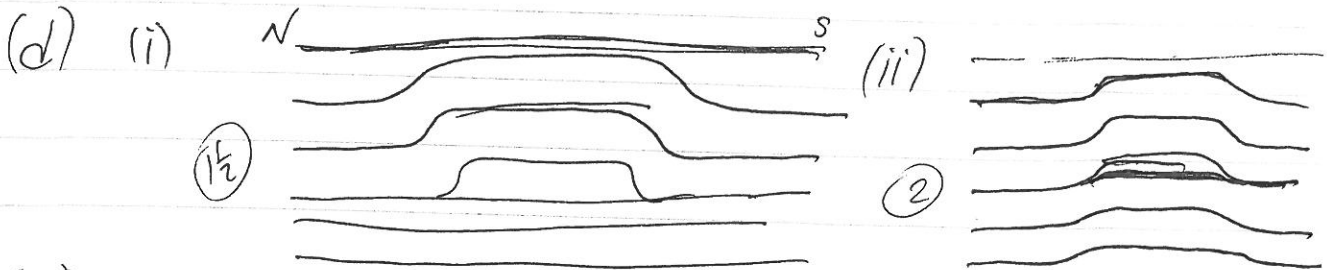
~~9 1/2~~



~~4 1/2~~



~~8 1/2~~



~~1/2~~

4 Fig. 1 (a) ~~Events~~ <sup>Events</sup> Horizons are not well resolved  
not very continuous

(3) (b) ~~Events~~ <sup>Events</sup> Horizons are well resolved, quite continuous  
Traces & events well aligned

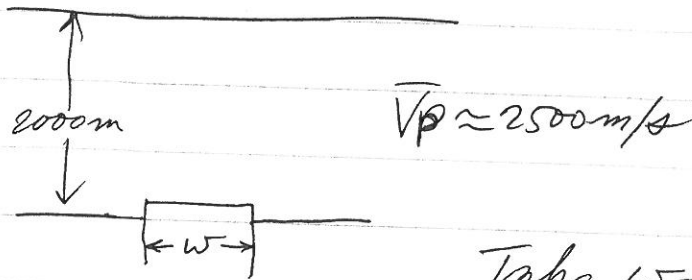
Statics  $-1/4$  for no  
1 for VSP\* (-1 for "2-way time")  
(-1/4 for downgoing)  
(-1/2 for no "upgoing")  
Fig. 2 (a) VSP traces w. downgoing attenuated  
i.e. upgoing field (except maybe  
dashed line of 1st breaks)  
(b) 2-way time [adding down-time to upgoing] TIME  
a sort of "NMO-correction"

(3) Fig. 3 (a) contains lot of ringing/reverberation  
(b) ringing removed (events can be seen)  
Deconvolution (1/2)

(3) Fig. 4 (a) Shot gather w. amplitude decreasing dra-  
stically w. depth/time (b) Amplitude boosted back  
Correction for geometric spreading/spherical  
divergence

(3) Fig. 5 (a) Low-V noise obscures <sup>high-V</sup> reflections. (1)  
(b) Low-V " attenuated, reflections (1/2)  
much more visible  
Vel'y Filtering -OR- spreading geophones for (b)  
f-k (1/2) clustered in (a)

4. (b)



Take  $w = w_F$ , Fresnel-zone width

In this limiting case

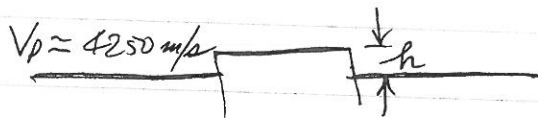
$$\lambda \doteq \frac{V_p}{f} = \frac{2500}{f} \quad w = w_F = \sqrt{2\lambda z} = 300 \text{ m} \quad z \doteq 2000 \text{ m}$$

$$\text{So } 300 = \sqrt{2 \times \frac{2500}{f} \times 2000}$$

$$\text{or } f = \frac{2 \times 2500 \times 2000}{300^2} = 111.1 \text{ Hz or } \sim 110 \text{ Hz}$$

So, to accomplish this resolution we need  $f \gtrsim 110 \text{ Hz}$

(c)



To resolve we need  $h \gtrsim \frac{\lambda}{4}$ .  $f \doteq 30 \text{ Hz}$

$$\lambda \doteq \frac{V_p}{f} = \frac{4250}{30} \quad \text{So } h \gtrsim \frac{4250}{120} \quad \text{or } h \gtrsim 35 \text{ m}$$

$$\lambda = 141.67 \text{ m}$$

(Taking the  $\frac{1}{2}$  criterion, we can resolve  $h \gtrsim 20 \text{ m}$ )