

PET565 PART B: EXERCISE SET 4

GOALS

- Become familiar with the analytical solution for tracer flow (advection + diffusion / dispersion)

IMPORTANT NOTES

The analytical solution is also implemented in a Matlab code ('tra_ads.m') which accounts for advection, dispersion and linear adsorption.

The analytical solution for advection and dispersion at a fixed boundary concentration c^{inj} and initial concentration c_i is given by equation (3.66), repeated below:

$$c(x, t) = c_i + \frac{c^{inj} - c_i}{2} \left[\operatorname{erfc}\left(\frac{x - vt}{\sqrt{4D_L t}}\right) + \exp\left(\frac{vx}{D_L}\right) \operatorname{erfc}\left(\frac{x + vt}{\sqrt{4D_L t}}\right) \right]$$

1. EXERCISES

1.1. Assume a brine with concentration $c_0 = 10\text{M}$ is injected into a core of 0.05 m length, containing brine with initial concentration $c_i = 5\text{M}$. The dominant mechanisms are dispersion and advection. Assume a dispersion coefficient $D_L = 1e - 4\text{m}^2/\text{hr}$ and water velocity of 0.05m/hr.

- Sketch the concentration profile after 0.5 hrs using equation (3.66). You can use Excel or the table with the *erfc* function or the Matlab code.
- Sketch the produced concentration at the outlet position $x = 0.05$ m as a function of injected pore volumes.
- Now let the dispersion coefficient be reduced to $D_L = 1e - 5\text{m}^2/\text{hr}$ (this makes dispersion less significant). What is the effect on the concentration profile?
- Now assume there is no advection by setting $v = 0$, and only diffusion. Show that equation (3.66) can be reduced to equation (3.58).
- In the case where only diffusion is present, plot the concentration profile after 5hrs using $D_L = 1e - 5\text{m}^2/\text{hr}$ (a representative diffusion coefficient). What is the difference compared to when advection is present?
- Calculate the time at which the concentration $c = 7.5$ reaches the outlet position $x = 0.05\text{m}$ for this case, using equation (3.58).

1.2. A brine is injected with 2 species (SCN^- and SO_4^{2-}) both having concentration $c^{inj} = 10\text{mM}$ into a core of 0.05 m length, and the initial concentrations are $c_i = 0\text{mM}$. The dominant mechanisms are dispersion and advection. The SO_4^{2-} species can adsorb, while SCN^- is a tracer. Assume a dispersion coefficient $D_L = 1e - 4\text{m}^2/\text{hr}$ and water velocity of 0.05m/hr. The porous cross section is 5 cm^2 .

- Assume the adsorbing species SO_4^{2-} has a linear isotherm $q = kc$. Plot the concentration profiles along the core after 1 hr assuming $k = 0.05, 0.25$ and 0.5 .
- Plot the produced concentration time profiles for the same cases during 2 injected pore volumes.
- Assume the case $k = 0.5$ corresponds to a water-wet core with residual oil, while the case $k = 0.05$ is for a strongly oil-wet core. Calculate the adsorbed amount of moles in each case after flooding the cores by
 - Integrating the difference in concentration time profiles,
 - and by calculating the amount of adsorbed species $q(c)$ in the core for a given concentration.
- Calculate the wettability index of the core.

$$\operatorname{erf}(\beta) = \frac{2}{\sqrt{\pi}} \int_0^\beta e^{-t^2} dt$$

$$\operatorname{erf}(-\beta) = -\operatorname{erf} \beta$$

$$\operatorname{erfc}(\beta) = 1 - \operatorname{erf}(\beta)$$

| β | $\operatorname{erf}(\beta)$ | $\operatorname{erfc}(\beta)$ |
|---------|-----------------------------|------------------------------|
| 0 | 0 | 1.0 |
| 0.05 | 0.056372 | 0.943628 |
| 0.1 | 0.112463 | 0.887537 |
| 0.15 | 0.167996 | 0.832004 |
| 0.2 | 0.222703 | 0.777297 |
| 0.25 | 0.276326 | 0.723674 |
| 0.3 | 0.328627 | 0.671373 |
| 0.35 | 0.379382 | 0.620618 |
| 0.4 | 0.428392 | 0.571608 |
| 0.45 | 0.475482 | 0.524518 |
| 0.5 | 0.520500 | 0.479500 |
| 0.55 | 0.563323 | 0.436677 |
| 0.6 | 0.603856 | 0.396144 |
| 0.65 | 0.642029 | 0.357971 |
| 0.7 | 0.677801 | 0.322199 |
| 0.75 | 0.711156 | 0.288844 |
| 0.8 | 0.742101 | 0.257899 |
| 0.85 | 0.770668 | 0.229332 |
| 0.9 | 0.796908 | 0.203092 |
| 0.95 | 0.820891 | 0.179109 |
| 1.0 | 0.842701 | 0.157299 |
| 1.1 | 0.880205 | 0.119795 |
| 1.2 | 0.910314 | 0.089686 |
| 1.3 | 0.934008 | 0.065992 |
| 1.4 | 0.952285 | 0.047715 |
| 1.5 | 0.966105 | 0.033895 |
| 1.6 | 0.976348 | 0.023652 |
| 1.7 | 0.983790 | 0.016210 |
| 1.8 | 0.989091 | 0.010909 |
| 1.9 | 0.992790 | 0.007210 |
| 2.0 | 0.995322 | 0.004678 |
| 2.1 | 0.997021 | 0.002979 |
| 2.2 | 0.998137 | 0.001863 |
| 2.3 | 0.998857 | 0.001143 |
| 2.4 | 0.999311 | 0.000689 |
| 2.5 | 0.999593 | 0.000407 |
| 2.6 | 0.999764 | 0.000236 |
| 2.7 | 0.999866 | 0.000134 |
| 2.8 | 0.999925 | 0.000075 |
| 2.9 | 0.999959 | 0.000041 |
| 3.0 | 0.999978 | 0.000022 |

FIGURE 1. Table for evaluation of the error and complementary error function