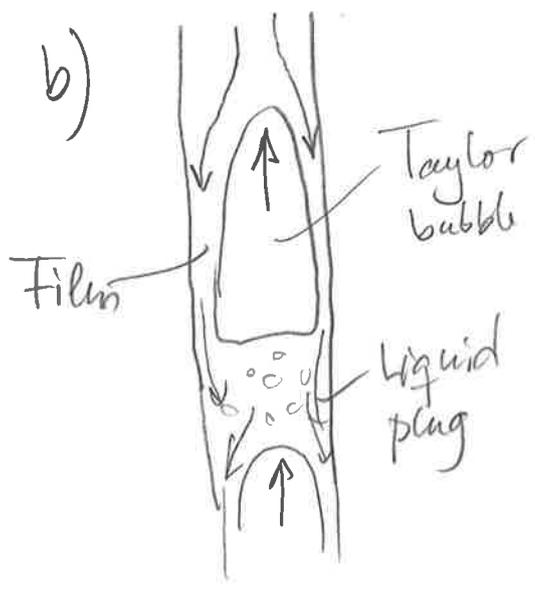
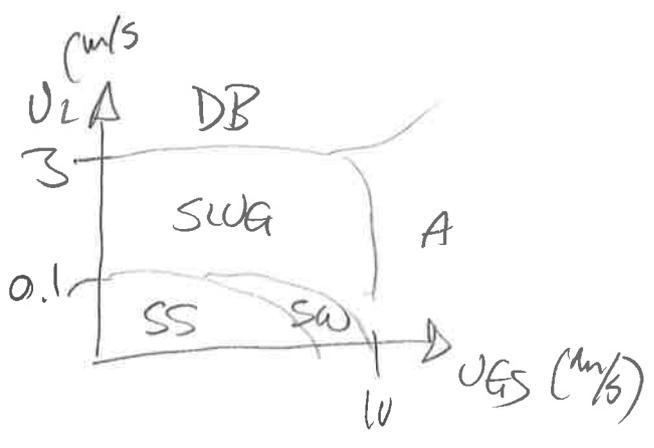
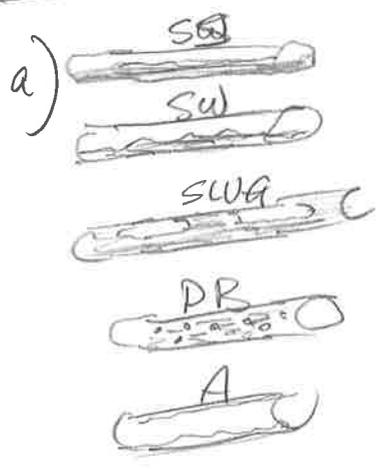


7/12-2016

SOLUTIONS PET 505 - 2016
MULTIPHASE FLOW PART -

(1)

PROBLEM 1



⇒ Yes, the bubble can move upwards, since the film is flowing counter to the bubble - downwards
 [As in lecture Nov. 9th]

c) Ideal gas $P \cdot V = n \cdot R \cdot T \Rightarrow P = \left(\frac{m}{V} \right) \cdot R \cdot T$ mol/volume \approx density

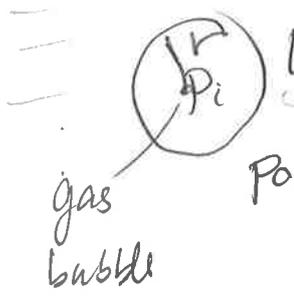
$\Rightarrow \rho_G(P, T) = \rho_{G, ref} \cdot \frac{P}{P_{ref}} \cdot \frac{T_{ref}}{T}$

$P = 5 \text{ bar}, T = 80^\circ\text{C} = (80 + 273.15)$

$T_{ref} = 25^\circ\text{C}$
 $P_{ref} = 1 \text{ bar}$

$\Rightarrow \rho_G(P, T) = \underline{5.07 \text{ kg/m}^3}$

When do we get an impact of surface tension, i.e. what diameter? (Or what is critical radius) ⁽²⁾



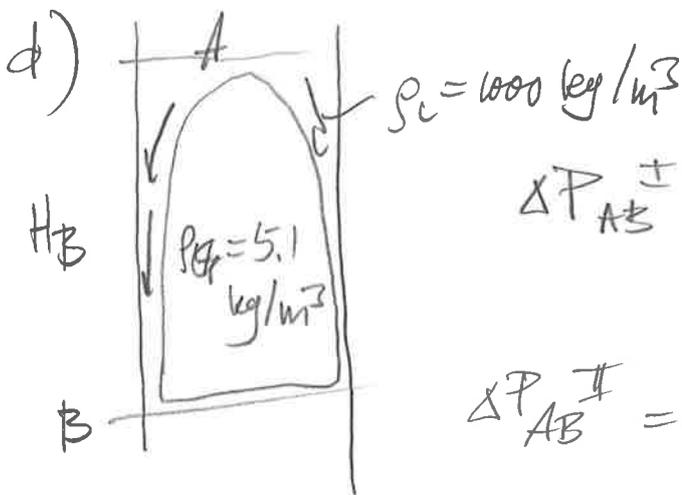
$$\Delta p = p_i - p_o = \frac{2\sigma}{r_{crit}} \Rightarrow r_{crit} = \frac{2\sigma}{\Delta p}$$

$$\Rightarrow r_{crit} = \frac{2 \cdot 72 \cdot 10^{-3} \text{ N/m}}{100 \cdot 10^{-3} \text{ bar}} = \frac{144 \cdot 10^{-3} \text{ N/m}}{10^4 \frac{\text{N}}{\text{m}^2}}$$

$$= 144 \cdot 10^{-7} \text{ m} = 144 \cdot 10^{-4} \text{ mm} = 1.44 \cdot 10^{-2} \text{ mm}$$

$$= \underline{1.44 \cdot 10^{-5} \text{ m}} = \underline{14.4 \mu\text{m}}$$

(= VERY SMALL!)



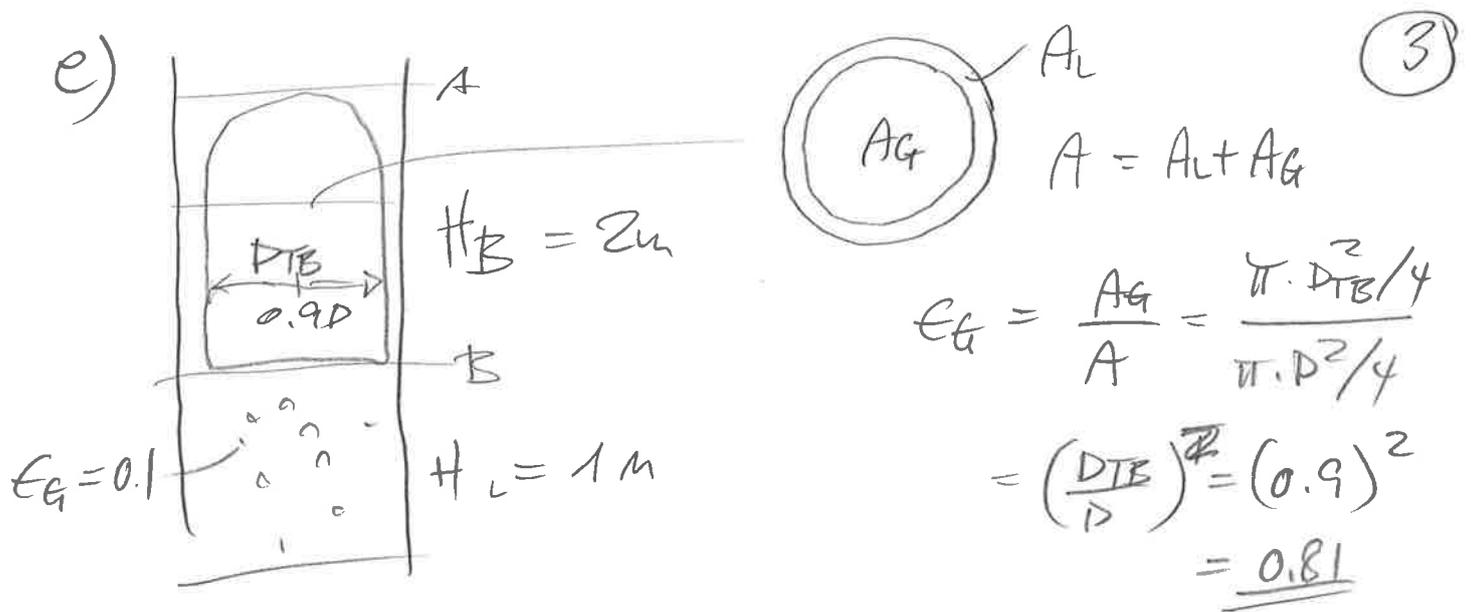
$$\Delta P_{AB}^I = \rho_l \cdot g \cdot H_B = 5.1 \cdot 9.81 \cdot 2 = 100 \text{ Pa} = 10^{-3} \text{ bar}$$

$$\Delta P_{AB}^{II} = \rho_c \cdot g \cdot H_B = 1000 \cdot 9.81 \cdot 2 = 19620 \text{ Pa} = 0.196 \text{ bar}$$

$\Rightarrow \Delta P_{AB}^{II} \sim 20 \cdot \Delta P_{AB}^I \Leftrightarrow$ PARADOX, since if P_A

is well defined to be $P_A = 5 \text{ bar}$, then the pressure P_B should also be well defined. But here we have two different P_B values.

The solution to the paradox is that friction in the down flowing film balances the hydrostatic "drive".



i) So, $\epsilon_{G_{TB}} = \frac{A_G}{A} = \underline{\underline{0.81}}$

ii) The homogeneous model says that

$$\begin{aligned} \Delta P_{hyd} &= \rho_{mix} \cdot g \cdot H_B \\ &= \underbrace{[\rho_L \cdot (1 - \epsilon_G) + \rho_G \cdot \epsilon_G]}_{194.1} \cdot 9.81 \cdot 2 \\ &= \underline{\underline{3.8 \cdot 10^3 \text{ Pa}}} \left[\sim 5.1 \cdot \Delta P_{AB}^{II} \right] \\ &\quad \text{Comparison} \end{aligned}$$

iii) We could get the total ΔP_{ABC} by

adding the extra hydrostatic contribution

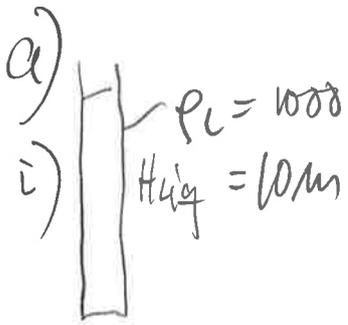
$$\begin{aligned} \Delta P_{BC} &= \rho_{mix} \cdot g \cdot H_L = (\rho_L \cdot 0.9 + \rho_G \cdot 0.1) \cdot 9.81 \cdot 1 \\ &= (1000 \cdot 0.9 + 500 \cdot 0.1) \cdot 9.81 \cdot 1 = 1.03 \cdot 10^3 \end{aligned}$$

$$\Rightarrow \Delta P_{AC} = \Delta P_{AB} + \Delta P_{BC} = 3.8 \cdot 10^3 + 1.03 \cdot 10^3 = 4.8 \cdot 10^3 \text{ Pa}$$

$$\left. \begin{array}{l} \text{AVERAGE PRESSURE GRADIENT} \\ \text{OVER THE SWG} \end{array} \right\} = \frac{\Delta P_{AC}}{H_B + H_L} = \frac{4.8 \cdot 10^3 \text{ Pa}}{3 \text{ m}} = 1.6 \cdot 10^3 \frac{\text{Pa}}{\text{m}}$$

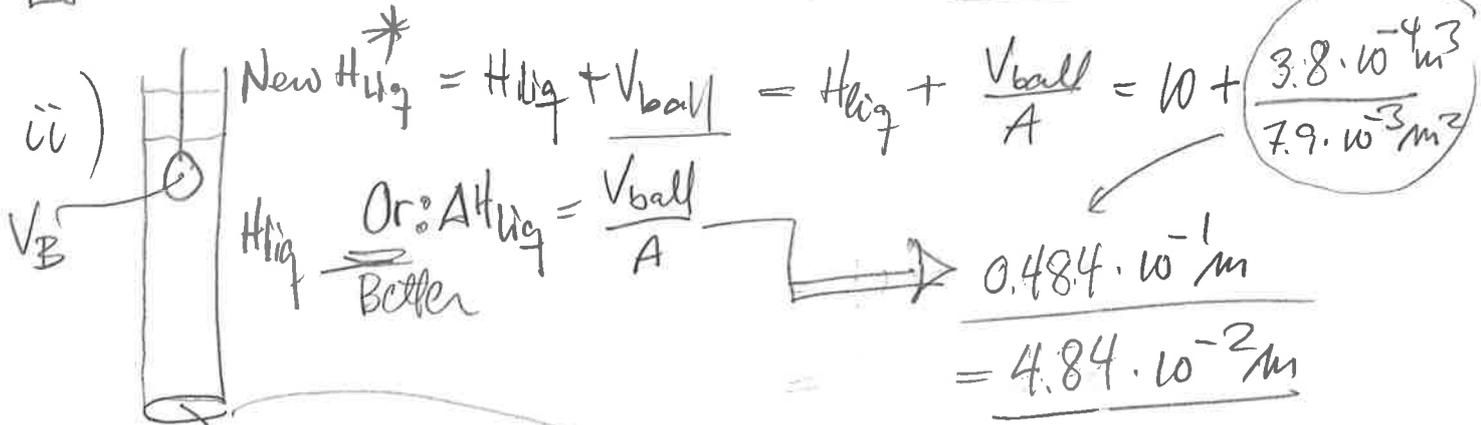
PROBLEM 2

(4)



$$\Rightarrow P_{\text{bottom}} = \rho_l \cdot g \cdot H_{\text{liq}} = 1000 \cdot 9.8 \cdot 10 = 9.8 \cdot 10^4 \text{ Pa}$$

$$= 0.98 \text{ bar}$$



$$A = \frac{\pi D^2}{4} = \frac{\pi \cdot 10^{-2}}{4} = 7.9 \cdot 10^{-3} \text{ m}^2$$

$$V_{\text{Ball}} = \frac{4}{3} \pi r^3 = \frac{4}{3} \pi \cdot \left(\frac{D}{2}\right)^3$$

$$= \frac{4}{3} \pi \cdot \frac{D^3}{8} = \frac{\pi D^3}{6} = \frac{\pi \cdot (0.09)^3}{6}$$

$$= 3.8 \cdot 10^{-4} \text{ m}^3$$

$$\Delta p = \rho_l \cdot g \cdot \Delta H_{\text{liq}}$$

$$= 10^3 \cdot 9.81 \cdot 4.84 \cdot 10^{-2}$$

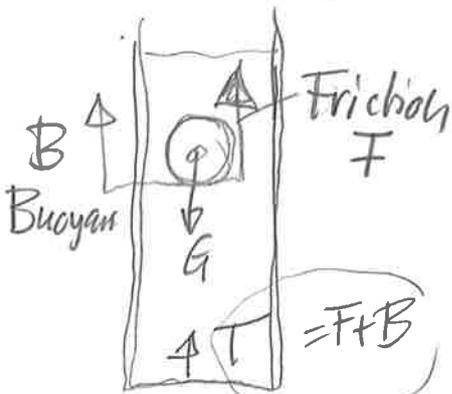
$$= 47.5 \cdot 10 \text{ Pa}$$

$$= 4.75 \cdot 10^2 \text{ Pa} \quad [10^2 \text{ Pa} = 1 \text{ mbar}]$$

$$= 4.75 \text{ mbar}$$

b) After some time the fall velocity is so high that friction + Buoyancy balances the gravitational force

\Rightarrow Sum of forces = 0 \Rightarrow constant fall velocity



Total force on Ball: $T = G - (F + B)$

The "counter" forces $F + B$ is set up by the fluid. To keep the fluid non-accelerated also, the bottom

%

takes the counter forces against the liquid.

(5)

⇒ So, yes, the pressure at the bottom now increases compared to a ii)!

$$c) \boxed{f_H = 4 \cdot f_F} \quad \left(\frac{dP}{dx}\right)_F = \frac{4}{D} \cdot f_F \cdot \frac{1}{2} \rho v^2$$

$$\left(\frac{dP}{dx}\right)_H = \frac{1}{D} \cdot f_H \cdot \frac{1}{2} \rho v^2$$

d) Testing the friction factors for some cases, making a table

	Re			
	5000	10000	10 ⁵	
a) $f_1 = 0.0056 + 0.5 \cdot Re^{-0.32}$ <small>Ptew, Koo, McAdam</small>	$3.84 \cdot 10^{-2}$	$3.18 \cdot 10^{-2}$	$1.82 \cdot 10^{-2}$	⇒ <u>Moody</u>
b) $f_2 = 0.052 \cdot Re^{-0.21}$	$8.7 \cdot 10^{-3}$	$7.5 \cdot 10^{-3}$	$4.6 \cdot 10^{-3}$	~ <u>Nester Fanning</u>
c) $f_3 = -1.8 \cdot \log_{10} \left(\frac{6.9}{Re}\right)$	5.1482	5.69	9.29	} <u>Fail!</u>
	$3.77 \cdot 10^{-2}$	$3.09 \cdot 10^{-2}$	$1.78 \cdot 10^{-2}$	
d) $f_4 = 0.36 \cdot Re^{-0.7}$	$6.55 \cdot 10^{-2}$	$5.71 \cdot 10^{-2}$	$3.6 \cdot 10^{-2}$	} <u>Fail!</u>
<u>Fanning</u> $f_{Publer} = 0.046 \cdot Re^{-0.2}$	$8.4 \cdot 10^{-3}$	$7.3 \cdot 10^{-3}$	$4.6 \cdot 10^{-3}$	} <u>Fail!</u>

a) is Moody b) Fanning c) & d) are wrong!