

25/18



University of
Stavanger

FACULTY OF SCIENCE AND TECHNOLOGY

SUBJECT: PET 535: MODERN WELL DESIGN

DATE: MAY 19, 2015

TIME: 0900 - 1300

AID: CALCULATOR

THE EXAM CONSISTS OF 6 PAGES

REMARKS: PLEASE STATE ASSUMPTIONS

Problem 1: Casing Design

You are asked to design a surface casing. The design parameters are as follows:

Depth of casing:	1100 m	800m 1000m
Depth to seabed:	225 m	110 m
Depth to sea level:	25 m	42 m
Depth to top of tail cement:	1000 m	900m
Depth to top lead cement:	225 m	
Depth next open hole section:	1820 m	3100m
Design fracture gradient at casing shoe:	1.57 s.g.	1,83
Pore pressure gradient, casing shoe:	1.03 s.g.	1,45
Pore pressure gradient, next section:	1.40 s.g.	
Formation fluid density:	0.76 s.g.	
Mud density:	1.20 s.g.	1,3
Mud density, next open hole section:	1.50 s.g.	1,7
Lead cement density:	1.45 s.g.	1,5
Tail cement density:	1.90 s.g.	1,9

The casing data are:

18-5/8 in. grade X-70, 84.5 lb/ft. casing	
Weight:	186 kg/m
Crosssectional inner area:	1527 cm ² .
Burst strength:	197 bar
Collapse resistance:	43 bar
Pipe body yield strength:	800 x 10 ³ daN

Remember to define the important assumptions.

- Prepare a drawing of the situation: the casing during installation. Define two criteria for casing collapse . Compute the design factor for these scenario.
- Prepare a drawing of the situation: the burst design. Define a burst scenario. Compute the design factor for burst.
- Define two scenarios for tension design. Compute the design factors.
- Compute the casing test pressure.
- Compute the kick margin of the casing section.
- Define the weak point in the well.

Problem 2: Geomechanics

- Show an expression for the horizontal in-situ stress. How would you select the mudweight relative to this? What do we call this concept?
- Three LOT data sets are given in a well as follows:

Depth(m):	LOT(s.g.):	Pore(s.g.):	Overburden(s.g.):	Inclination(°):
890	1,51	1,03	1,62	0
1124	1.35	1.21	1.76	30
1540	1,27	1,30	1,80	39

Estimate the LOT values for vertical hole sections.

- Compute the horizontal stress levels from the data above. State all assumptions.

Problem 3: Fundamentals

Please identify the most correct answer below. Just write answer number, f.eks. a1, b1, and so on.

- a) Which equilibrium condition dominate geomechanics:
 - 1) Stress equilibrium
 - 2) Newtons 2nd law
 - 3) Maxwell equations
 - 4) Conservation of mass

- b) Which statement is correct:
 - 1) The dog leg is the vertical angle
 - 2) The DLS act in the vertical plane
 - 3) The DLS is a 3 dimensional parameter
 - 4) The DL is the derivative of the angle

- c) Stresses transforms in space according to:
 - 1) Linearly
 - 2) Squared trigonometric law
 - 3) Cubic trigonometric law
 - 4) None of the above

- d) Replacing the mud in the drill string with sea water leads to:
 - 1) Reduction in surface pipe tension
 - 2) Increase in surface pipe tension
 - 3) No change in surface pipe tension
 - 4) Differential sticking

- e) Surface casing is installed:
 - 1) Through the marine riser
 - 2) Before riser is installed
 - 3) Through the BOP
 - 4) After riser is installed

- f) On jack-up rigs
 - 1) Always implement riser margin
 - 2) New rigs uses dynamic positioning
 - 3) Have the weight of the well on mud line suspension system
 - 4) Can work in 200 m of water

- g) Wellhead systems
 - 1) Horizontal X-mas trees are mostly used subsea
 - 2) Vertical X-mas trees are mostly used subsea
 - 3) BOP is mainly used during production of the well
 - 4) One well barrier is sufficient for low pressure wells

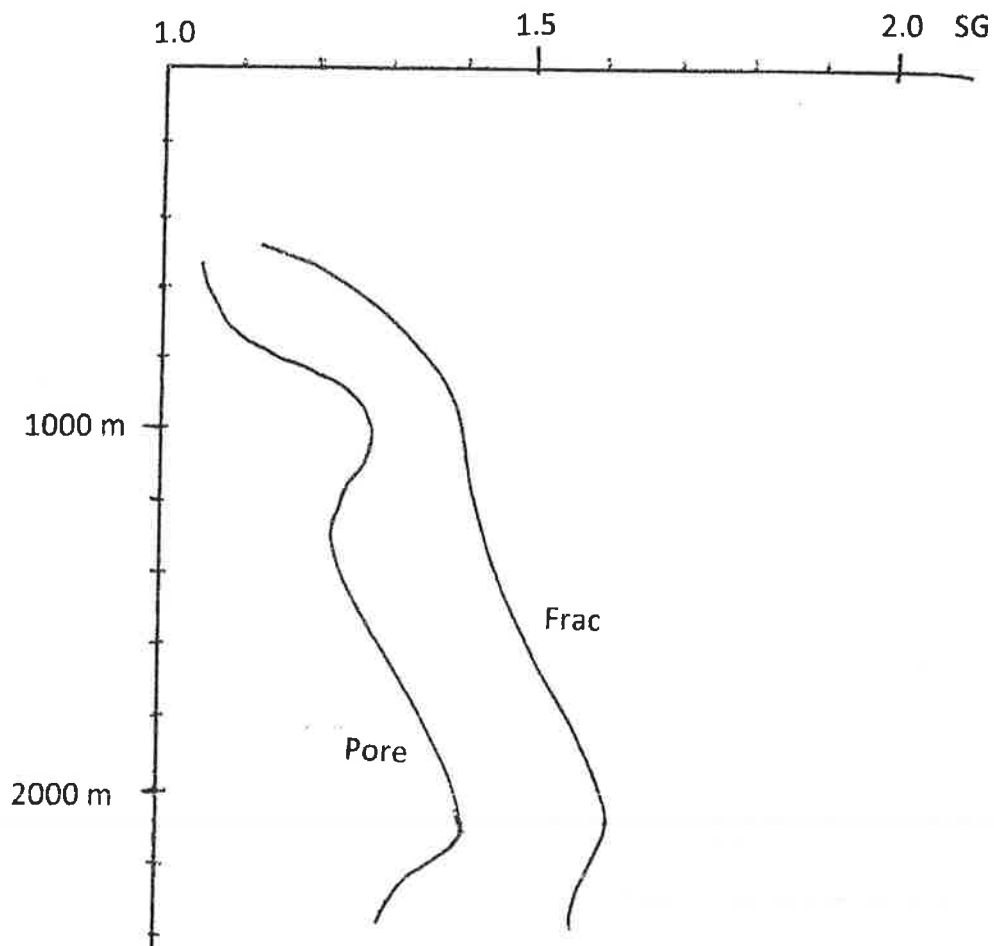
Problem 4: Casing depth and mud weight selection

a) Using the gradient curve below propose the depth of the following casings:

- 7 in liner
- 9-5/8 in production casing
- 13-3/8 in intermediate casing
- 20 in surface casing
- 30 in conductor casing

b) Propose a mud weight program for the well. Define assumptions.

You can draw directly on the figure below and include this page in your exam.



c) Consider implementing a riser margin. Is this possible? Explain!

Problem 5: Data normalization

You are planning a subsea infill well in a production field. Your design is based on data from the production platform which has a wellhead elevation of 120 m. You are going to use a jackup drilling rig with a air gap of 40 m. The water depth is 300 m. The data from the production platform are:

Pore press.	0.82	0.90	0.95	1.10	1.15	1.20
Grad.(sg)						
Depth(m)	500	700	900	1100	1300	1500

- a) Define the normalization equations.
- b) Normalise the pore pressure gradient to drillfloor level and sea level. Show all three curves in a plot.
- c) Connect each data point with a curve for the three reference levels. Explain the meaning of this curve. What do we call this curve?

Some Formulas

$$P(\text{bar}) = 0.098 \times d(\text{s.g.}) \times D(\text{m})$$

$$P_3 = Cq^m$$

$$P_2 = \rho q^2 / 2A^2 \cdot 0.95^2$$

Index:	Equation:	Criterion:	Fraction parasitic pressure loss:	Flow rate:
1	$q\sqrt{P_2}$	Max. HP	$1/(m+1)$	$P_1/C(m+1)$
2	$q\sqrt[3]{P_2}$	Max. jet impact	$2/(m+2)$	$2P_1/C(m+2)$
3	$q^{3/2}\sqrt{P_2}$	New A	$3/(m+3)$	$3P_1/C(m+3)$
4	$q^2\sqrt[3]{P_2}$	New B	$4/(m+4)$	$4P_1/C(m+4)$
5	$q^{5/2}\sqrt{P_2}$	New C	$5/(m+5)$	$5P_1/C(m+5)$

$$A = q \{ \rho / 2P_2 \}^{1/2} / 0.95$$

Using the units of: density(kg/l), flowrate (l/min) and pressure (bar), the nozzle area in in² can be obtained by dividing the equation above with 122.4.

$$d_{\text{RKB1}} = d_{\text{RKB2}} D / (D - \delta h)$$

$$\text{LOT} = 2\sigma_a - P_o$$

$$P_{\text{wf}}(\gamma) = P_{\text{wf}}(0) + 1/3 (P_o - P_o^*) \sin^2 \gamma$$

$$P_{\text{wf}}(0) = \{ P_{\text{wf}}(\gamma) + (\sigma_o - 1/2 P_o) \sin^2 \gamma \} / \{ 1 + 1/2 \sin^2 \gamma \}$$

$$\Delta\sigma_a = \Delta P_o (1 - 2v) / (1 - v)$$

$$\Delta P_{\text{wf}} = \Delta P_o (1 - 3v) / (1 - v)$$

$$P_{\text{burst}} = 2\sigma_{\text{tensile}} t / D_o$$

$$P_{\text{collapse}} = \{ 2CE / (1 - v^2) \} \{ 1 / (D_o/t - 1)^2 D_o/t \}$$

$$(\sigma_t / \sigma_{\text{yield}}) = 1/2 (\sigma_a / \sigma_{\text{yield}}) + / - \{ 1 - 3/4 (\sigma_a / \sigma_{\text{yield}})^2 \}^{1/2}$$

$$\rho = (d_p D - 1.03 h_w) / (D - h_f - h_w)$$

$$d_{\text{wf2}} = d_{\text{wf1}} \frac{D_1}{D_2} + d_{\text{sw}} \frac{D_{\text{w2}} - D_{\text{w1}}}{D_2}$$

$$D_2 = D_1 + (D_{\text{w2}} - D_{\text{w1}}) + (D_{\text{f2}} - D_{\text{f1}})$$