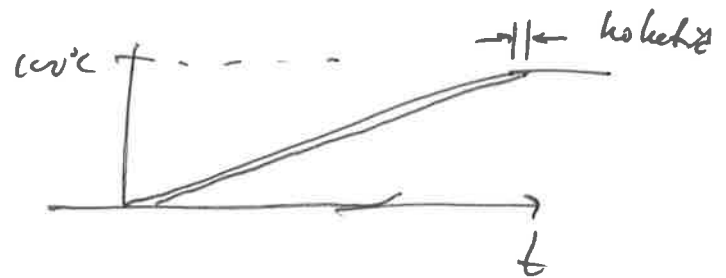
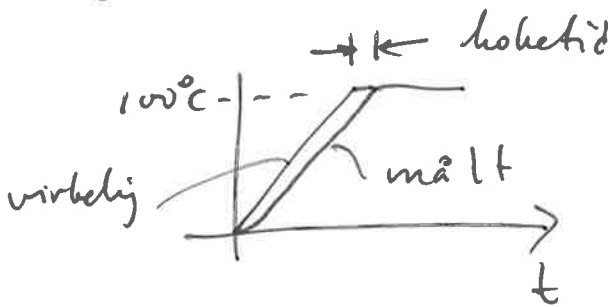


Løsningsforslag ELE320 Reg. tek ⑫

3. mai 2018

Oppg 1

- a) Under oppvarming vil det pga dynamikk i temperaturføleren være en forskjell mellom virkelig temperatur i vannet og målt temperatur. Denne forskjellen er størst når temperaturstigningen skjer raskt (lite vann). Derfor vil det ta lenger tid ved oppvarming av lite vann.



b)

$$\frac{dE(t)}{dt} = Q_{in}(t) = P(t)$$

$$E(t) = m \cdot c_p \cdot T(t)$$

$$m \cdot c_p \cdot \frac{dT(t)}{dt} = P(t) \Rightarrow \frac{dT(t)}{dt} = \frac{1}{m \cdot c_p} \cdot P(t)$$

c) Dette er en integrator prosess.

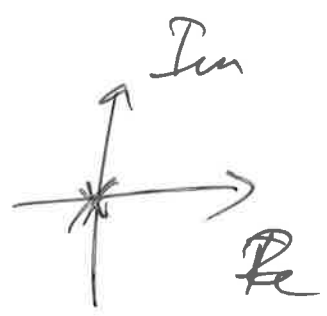
Vannet akkumulerer all tilført energi, taper ingenting

$$d) \mathcal{L} \left\{ \dot{T}(t) = \frac{1}{mcp} P(t) \right\}$$

$$s T(s) = \frac{1}{mcp} \cdot P(s)$$

$$H_p(s) = \frac{T(s)}{P(s)} = \frac{\frac{1}{mcp}}{s} = \frac{1}{m \cdot c_p \cdot s}$$

e) $m \cdot c_p \cdot s = 0$, $\Rightarrow s = 0$
pol i origo
 \Rightarrow integrator



f) ved å gi en inputs får vi

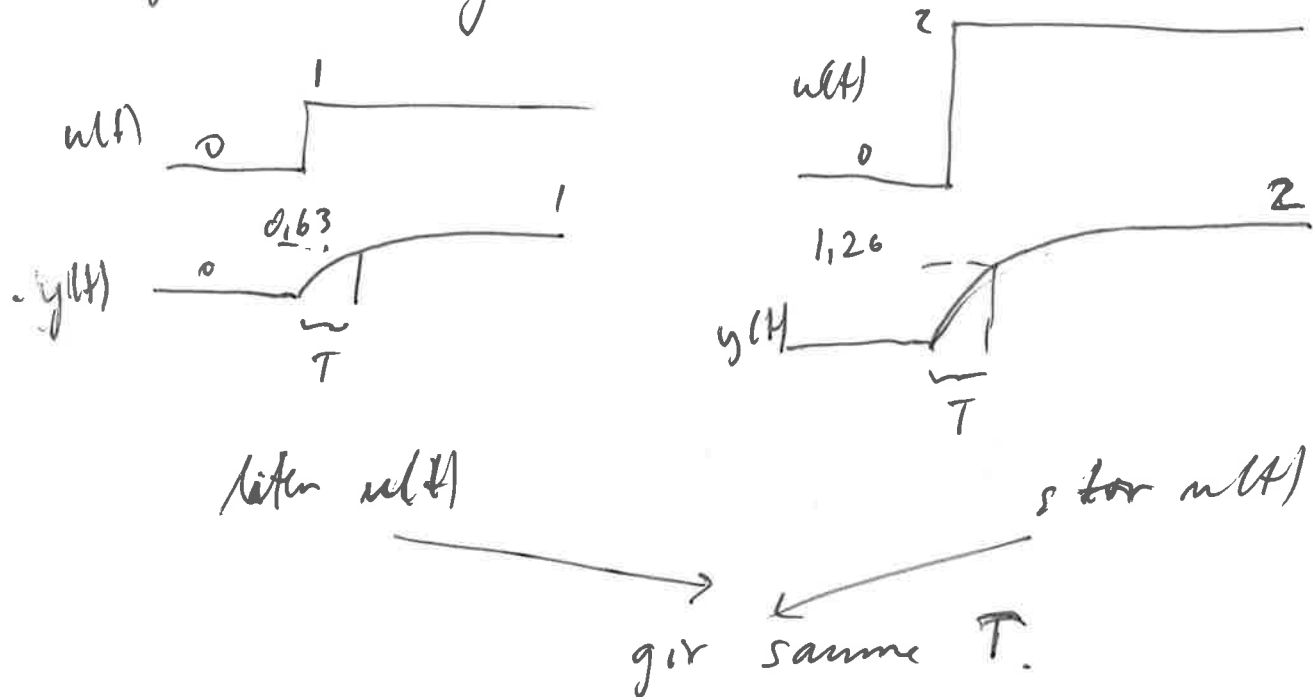
$$T(s) = H_p(s) \cdot P(s)$$

$$\lim_{t \rightarrow \infty} T(t) = \lim_{s \rightarrow 0} \underbrace{\frac{1}{mcp \cdot s}}_{H_p(s)} \cdot \underbrace{1}_{\mathcal{L}\{s(t)\}} = \frac{1}{mcp}$$

Dette er mellom 0 og $\infty \Rightarrow$ marginalt stabilt

g) Tidskonstanten vil være uafhængig af temperaturen på vandet.

Detta fordi tidskonstant er en system-egenskab, og ikke afhængig af styrken i $u(t)$



h) $\Delta y = 60 - 20 = 40^\circ\text{C}$

63% af $40^\circ\text{C} = 25,2^\circ\text{C}$

Ablest ved $T(t) = 20 + 25,2 = 45,2$,

finder vi $t = 6$ sek und. Sprøjtet

går ved $t = 4$ sek \Rightarrow Tidskonstant

$T_m = 2$ sek

$H_m(s) = \frac{1}{2s + 1}$

i) $T(s) = \frac{1}{2 \cdot 4200 \cdot s} \cdot P(s)$

$$= \frac{1.2 \cdot 10^{-4}}{s} P(s)$$

hvor $P(s) = \frac{P}{s}$

$$= \frac{1.2 \cdot 10^{-4} \cdot P}{s^2} \quad 23!$$

Prøver lign (22) i vedlegg

$$T(t) = \underbrace{1.2 \cdot 10^{-4} \cdot P \cdot t}_{\text{stigning}}$$

Stigningen avlest på $t=60 \rightarrow t=100$
 er på $12^\circ \rightarrow 21^\circ \approx \underline{\underline{9^\circ}}$

$$\text{stigning} = \frac{9^\circ}{40 \text{ sek}} = 1.2 \cdot 10^{-4} \cdot P$$

$$P = 1890 \text{ W} \approx 1900 \text{ W}$$

(5)

$$j) P = U \cdot I = 220 \cdot 10 = 2200 \text{ W}$$

$$\text{Dun} + \text{varmekar} = 1000 + 1900 = 2900 \text{ W}$$

Ja, den vil slå ud.

b) Responsen mellem $t = 20$ og $t = 80$ skyldes dynamikken i varmeelement og temp. transmitter.

Opp2

$$a) u(t) = k_p e(t) + \frac{k_p}{T_i} \int e(t) dt$$

Herp lace giv

$$u(s) = \left(k_p + \frac{k_p}{T_i s} \right) e(s)$$

$$\Rightarrow H_r(s) = \frac{u(s)}{e(s)} = \frac{k_p (T_i s + 1)}{T_i s}$$

(6)

b)

$$H_p(s) = \frac{0.23}{s+0.1} \Rightarrow \frac{2.3}{10s+1}$$

$$T=10, \quad K=2.3$$

$$T_c = \frac{10}{4} = \underline{2.5 \text{ sek}}, \quad k_f = 1.44$$

$$K_p = \frac{T}{KT_c} = \frac{10}{2.3 \cdot 2.5} = 1.73$$

$$T_i = \min(T, k_f \cdot T_c) = \min(10, 1.44 \cdot 2.5) \\ = \underline{3.6 \text{ sek}}$$

c)

$$H_m(s) = 1$$

$$M(s) = \frac{H_d(s)}{1+H_b(s)} = \frac{H_r \cdot H_p}{1+H_r \cdot H_p} = \frac{\frac{2.3}{10s+1} \cdot \frac{1.73(3.6s+1)}{3.6s}}{1 + \frac{2.3}{10s+1} \cdot \frac{1.73(3.6s+1)}{3.6s}}$$

$$= \frac{2.3 \cdot 1.73(3.6s+1)}{(10s+1)3.6s + 2.3 \cdot 1.73(3.6s+1)}$$

$$= \frac{4(3.6s+1)}{36s^2 + 3.6s + 14.3s + 4}$$

$$= \frac{4(3.6s+1)}{36s^2 + 17.9s + 4}$$

$$36s^2 + 3.6s + 14.3s + 4$$

$$M(s) = \frac{3,6 s + 1}{9s^2 + 4,5s + 1}$$

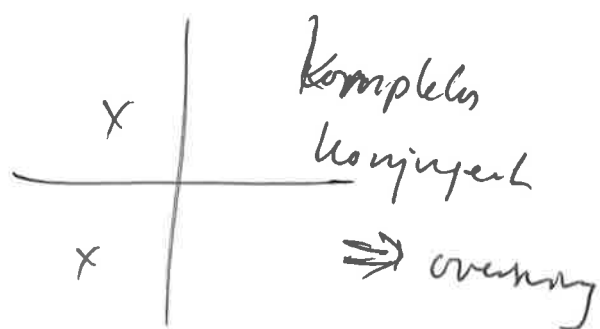
7

$$d) \quad 9s^2 + 4,5s + 1 = 0$$

$$s = \frac{-4,5 \pm \sqrt{4,5^2 - 4 \cdot 9}}{2 \cdot 9}$$

$$= \frac{-4,5 \pm j\sqrt{15,75}}{18}$$

$$= -0,25 \pm j 0,22$$



skizze neben son

$$\frac{s^2}{\omega_0^2} + \frac{2\zeta}{\omega_0} s + 1$$

$$\frac{1}{\omega_0^2} = 9$$

$$\frac{2\zeta}{\omega_0} = 4,5$$

\Downarrow

$$\omega_0 = \frac{1}{\sqrt{9}} = \frac{1}{3}$$

$$\zeta = \frac{4,5 \cdot \frac{1}{3}}{2} = 0,75 \Rightarrow \underline{\underline{\delta = 3-4\%}}$$

little overshoot

$$T_r \approx \frac{1,5}{\omega_0} \approx 4,5 \text{ sek} \Rightarrow \text{endel störrer am } T_c = 2,5$$

e) Nullpunktet i $M(s)$ vil gøre
responsen raske \Rightarrow mer like T_c .

f) $y(s) = M(s) \cdot y_r(s)$, $y_r(s) = \frac{1}{s}$

$$\lim_{t \rightarrow 0} y(t) = \lim_{s \rightarrow 0} s \cdot y(s) = \lim_{s \rightarrow 0} s \cdot M(s) \cdot \frac{1}{s}$$

$$= \lim_{s \rightarrow 0} M(s)$$

$$= M(0)$$

$$= \frac{1}{0 + 0 + 1} = 1$$

Reg. overhet $e = y_r - y = 1 - 1 = 0$

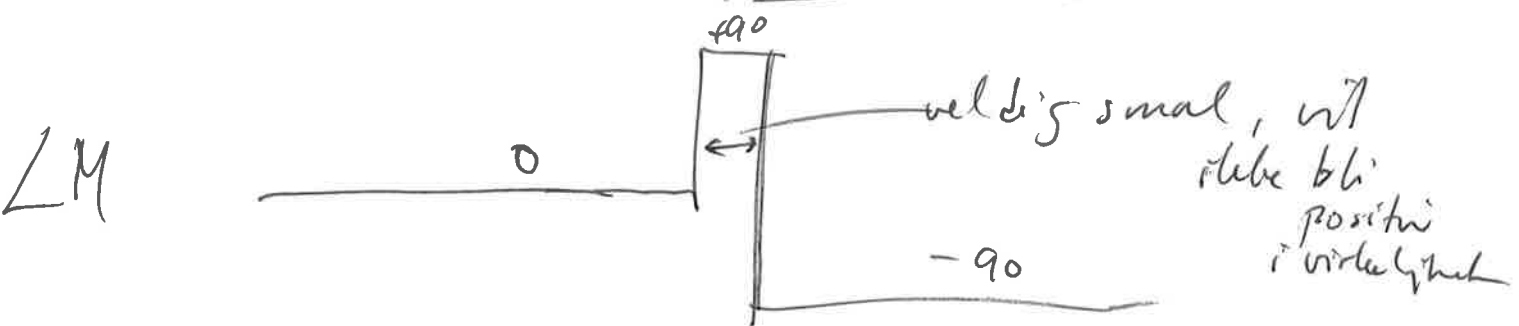
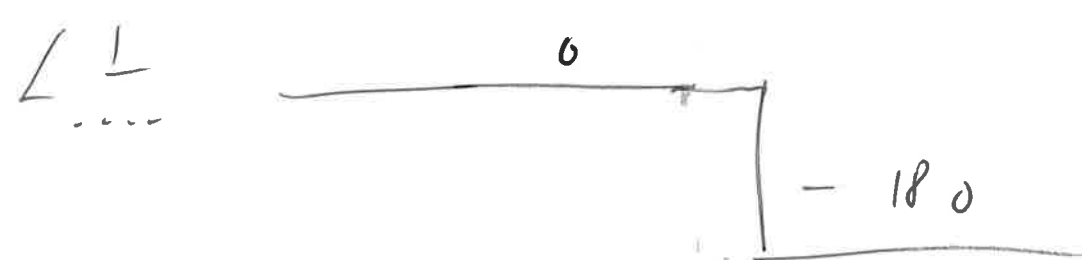
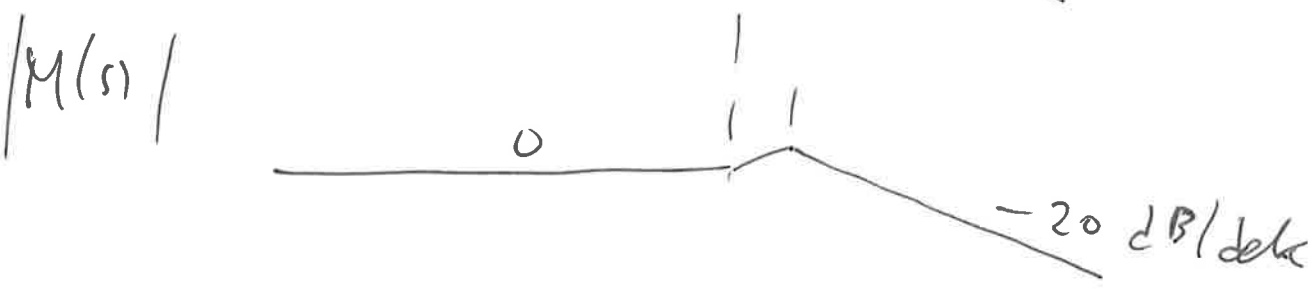
g) $\Delta K = \infty$

$$\varphi = 180 - 110 \approx 70^\circ$$

9

h) $M(s) = \frac{3.6s + 1}{9s^2 + 4.5s + 1}$

$\omega_0 = 0.33$ $\frac{1}{T} = \frac{1}{3.6}$ ω_0
 $0.27 \quad 0.33$



$$i) \quad M(j\omega) = \frac{3.6j\omega + 1}{9(j\omega)^2 + 4.5j\omega + 1}$$

$$= \frac{1 + j 3.6\omega}{(1 - 9\omega^2) + j 4.5\omega}$$

$$|M(j\omega)| = \frac{\sqrt{1 + 3.6^2 \omega^2}}{\sqrt{(1 - 9\omega^2)^2 + 4.5^2 \omega^2}}$$

$$\angle M(j\omega) = \text{atan}(3.6\omega) - \text{atan}\left(\frac{4.5\omega}{1 - 9\omega^2}\right)$$

$$j) \quad y_r(t) = 0.7 \sin(0.1 t) \quad \omega = 0.1$$

$$|M(j0.1)| = \frac{\sqrt{1 + 3.6^2 \cdot 0.1^2}}{\sqrt{(1 - 9 \cdot 0.1^2)^2 + 4.5^2 \cdot 0.1^2}} = \frac{1.06}{1.015}$$

$$= 1.046$$

$$\angle M(j0.1) = \text{atan}(0.36) - \text{atan}\left(\frac{0.45}{1 - 0.09}\right) = \underline{-6.5^\circ}$$

(11)

$$j) \quad y(t) = 0.7 \cdot 1.046 \cdot \sin(0.1t - 6.5) \\ \underline{\underline{= 0.73 \cdot \sin(0.1t - 6.5^\circ)}}$$

$$k) \quad \left. \begin{array}{l} |N(j\omega)| = -20 \text{ dB} \\ \angle N(j\omega) = 80^\circ \end{array} \right\} \text{ ved } \underline{\omega = 0.02}$$

folken 1: (i forbindelse med følgeegensluper)

$$N(s) = \frac{e(s)}{y_r(s)} \Rightarrow e(s) = N(s) \cdot y_r(s)$$

↑ sinus her

$$|N(j\omega)| = -20 \text{ dB} \Rightarrow 0.1$$

amplituden i reg. variabel $e(t)$ kommer til at være 0.1 af amplituden til $y_r(t)$, og 80° foran i fase.

folken 2: (i forbindelse med kompenjeringsluper)

$$N(s) = \frac{e_{\text{med reg}}(s)}{e_{\text{uden reg}}(s)}$$

med sinus i $v(t)$

