

9. des 2009

①

Løsningsforslag
BIE 240 Regtel

1) a) orden 2 for varmløser (varmefluid + vann)
orden 1 for stekte termometer
(stelekopling)

$K_m = 1$ fordi ~~ikke~~ stekte termometeret
er jo temperatur

$$H_m(s) = \frac{T_{m\ddot{o}lt}(s)}{T_{vann}(s)}$$

Vannet er tydelig varmet opp til 25.5°C

$$\Delta T = 25.5 - 18 = 7.5^\circ\text{C}$$

$$63\% \text{ av } 7.5^\circ\text{C} = 4.72^\circ\text{C}$$

~~Løser~~ Løser av fisen ved $18 + 4.72 = 22.7^\circ\text{C}$

$$T = 9 \text{ sek} - 4 \text{ sek} = 5 \text{ sek} \quad (\text{sprang gitt ved } \pm 4 \text{ sek})$$

$$4) H_m(s) = \frac{1}{ss+1}$$

(2)

$$5) \frac{dE(t)}{dt} = Q_i(t) - Q_{out}(t)$$

$$E(t) = m \cdot c_p \cdot T(t) \quad \text{(constant mass } m \text{ of } c_p \text{ liquid)}$$

$$m \cdot c_p \cdot \frac{dT(t)}{dt} = P(t) - hA(T(t) - T_{\infty}(t))$$

$$\frac{dT(t)}{dt} = \frac{1}{m c_p} (P(t) - hA(T(t) - T_{\infty}(t)))$$

Laplace

$$s \cdot T(s) = \frac{1}{m c_p} (P(s) - hA(T(s) - T_{\infty}(s)))$$

$$\left(s + \frac{hA}{m c_p}\right) T(s) = \frac{1}{m c_p} P(s)$$

$\ll K$

$$H_p(s) = \frac{T(s)}{P(s)} = \frac{\frac{1}{m c_p}}{s + \frac{hA}{m c_p}} = \frac{\frac{1}{hA}}{\frac{m c_p}{hA} s + 1}$$

τ

c) $m = 0.1$

$C_p = 4000$

$T_r \text{ anleset} : \cancel{23} \approx 23^\circ\text{C} - 18^\circ\text{C} = 5^\circ\text{C}$

$63\% \text{ an } 5 = 3.15^\circ\text{C}$

$18 + 3.15 = 21.15^\circ\text{C}$ an leses wert

$t = 35 \text{ sek}$

sprunget gleich
wert $t = 10$

$T_r \approx 35 - 10 = 25 \text{ sek.}$

$T_r \approx T_m + T$

$25 \approx 5 + \frac{m \cdot C_p}{hA}$

$hA = \frac{m \cdot C_p}{20} = \frac{0.1 \cdot 4000}{20} = 20$

$K = \frac{1}{20} = 0.05$

$T = 20 \text{ sek}$

$H_p = \frac{T(s)}{P(s)} = \frac{0.05}{20s + 1}$

(4)

$$d) H_{sys}(s) = \frac{1}{5s+1} \cdot \frac{0.05}{20s+1}$$

$$|H_{sys}(j\omega)| = \left| \frac{1}{1+j\omega 5} \cdot \frac{0.05}{1+j\omega 20} \right|$$

$$= \frac{0.05}{\sqrt{1+\omega^2 5^2} \cdot \sqrt{1+\omega^2 20^2}}$$

$$\angle H_{sys}(j\omega) = -\arctan(\omega 5) - \arctan(\omega 20)$$

e) $\omega = 0.01$

(5)

$$|H_{sys}(j0.01)| = \frac{0.05}{\sqrt{1+0.01^2 \cdot 5^2} \cdot \sqrt{1+0.01^2 \cdot 20^2}} = \underline{\underline{0.049}}$$

$$\angle H_{sys}(j0.01) = -\arctan(0.01 \cdot 5) - \arctan(0.01 \cdot 20) \\ = \underline{\underline{-14.17^\circ}}$$

$$|H_{sys}(j0.1)| = \frac{0.05}{\sqrt{1+0.1^2 \cdot 5^2} \cdot \sqrt{1+0.1^2 \cdot 20^2}} = \underline{\underline{0.02}}$$

$$\angle H_{sys}(j0.1) = -\arctan(0.1 \cdot 5) - \arctan(0.1 \cdot 20) \\ = \underline{\underline{-90^\circ}}$$

$$|H_{sys}(j1)| = \frac{0.05}{\sqrt{1+5^2} \cdot \sqrt{1+20^2}} = 4.9 \cdot 10^{-4}$$

$$\angle H_{sys}(j1) = -\arctan(5) - \arctan(20) \\ = \underline{\underline{-165^\circ}}$$

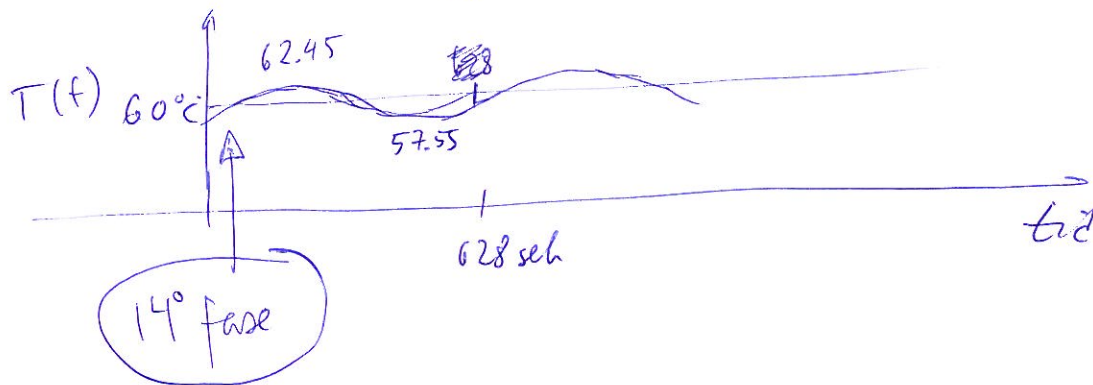
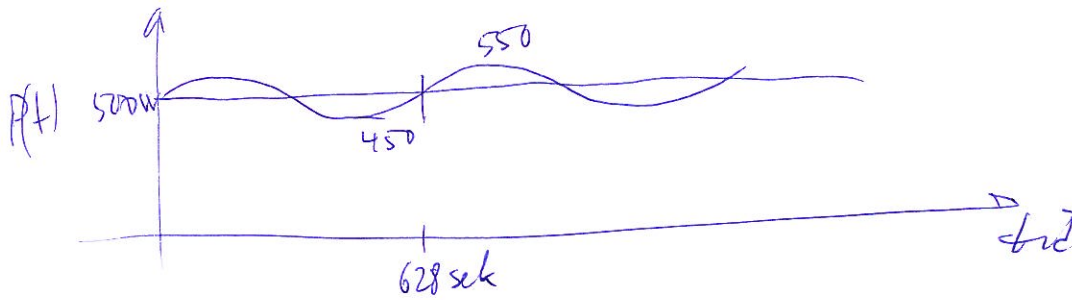
f) $\omega = 0.01 \text{ rad/sec}$

6

$$T_p = \frac{2\pi}{\omega} = \frac{6.28}{0.01} = 628 \text{ sek}$$

Amplitude i
temp. sinus:

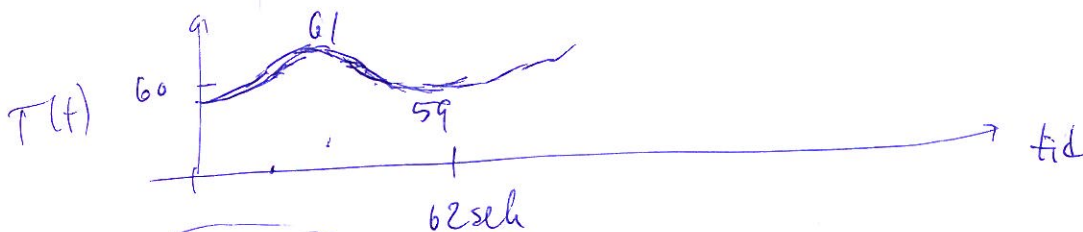
$$50W \cdot 0.049 = \underline{2.45^\circ}$$



$\omega = 0.1 \text{ rad/sec}$

$$T_p = \frac{2\pi}{\omega} = 62.8 \text{ sek}$$

Amplitude i temp. sinus
 $50W \times 0.02 = 1^\circ$



90° fase

f) $\omega = 1.0$ $T_p = \frac{2\pi}{\omega} = 6.28 \text{ sek}$

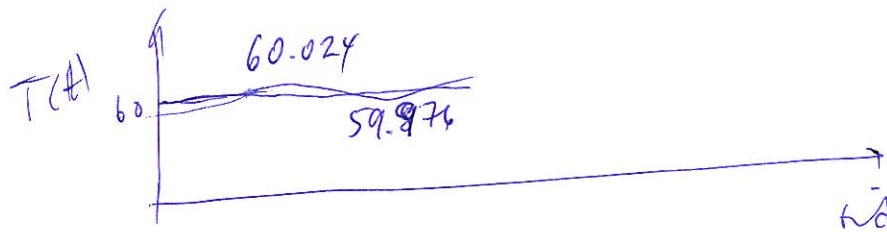
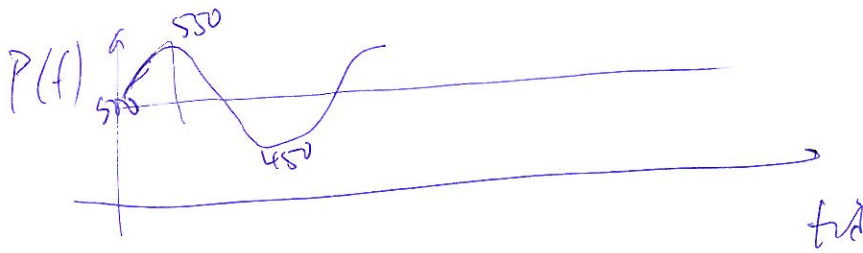
Amplitude i

Sinus :

$$50 \text{ W} \times 4.9 \cdot 10^{-4}$$

$$= \underline{0.024^\circ \text{C}}$$

(7)



2 Regulierung

(8)

$$a) \quad H_p(s) = \frac{0.2}{15s+1} e^{-2s}$$

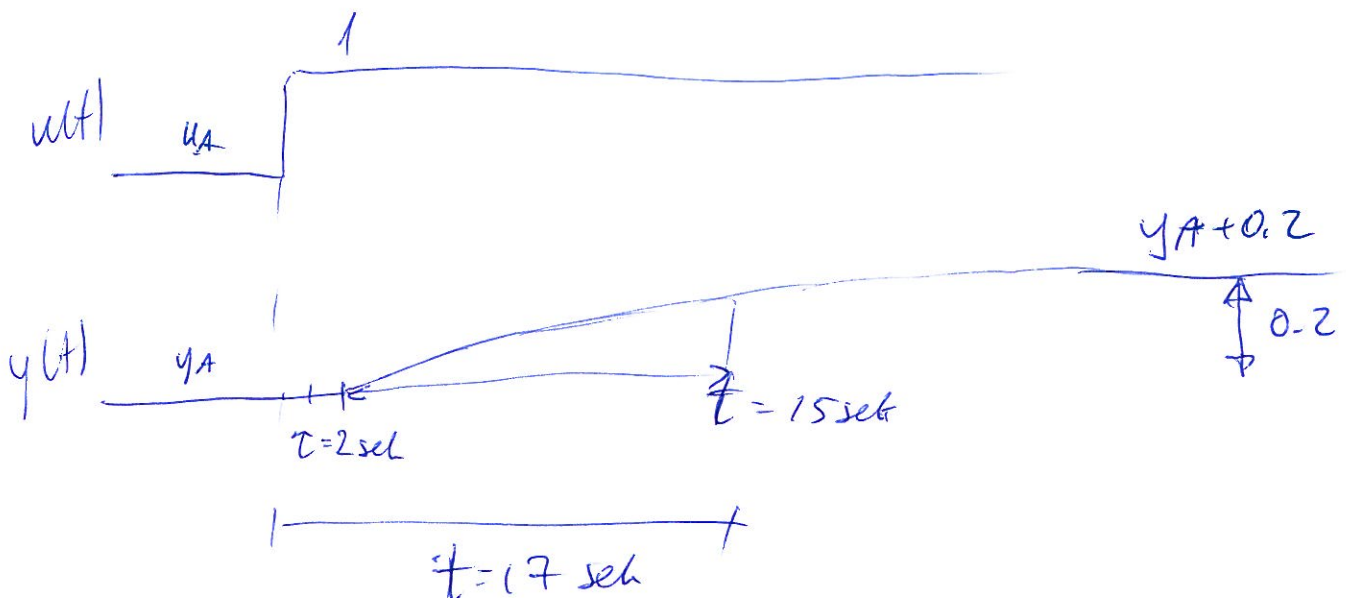
$$p = -\frac{1}{T} = -\frac{1}{15}$$

asymptotische Stabilität

$$\left\{ u(t) = k_p \cdot e(t) + \frac{k_p}{T_i} \int_0^t e(\tau) d\tau \right\}$$

$$u(s) = k_p e(s) + \frac{k_p}{T_i} \cdot e(s) \cdot \frac{1}{s}$$

$$H_r(s) = \frac{\bar{u}(s)}{e(s)} = k_p + \frac{k_p}{T_i s} = \frac{k_p T_i s + k_p}{T_i s}$$



$$b) K_p = \frac{0.9 \cdot V}{L \cdot R} = \frac{0.9 \cdot 4}{2 \cdot \frac{K \cdot 4}{T}} = \frac{0.9 T}{2 K} \quad (10)$$

$$T_i = 3.3 \cdot L = 3.3 \cdot 4$$

$$K_p = \frac{0.9 \cdot 15}{2 \cdot 0.2} = 33.75$$

$$T_i = 3.3 \times 2 = 6.6$$

$$c) H_p(s) = \frac{0.2}{15s+1}$$

1) Polplacering $\zeta = 0.6 \Rightarrow \delta = 0.1$ 10% overring

$$\omega_0 \approx \frac{1.5}{T_r} \approx \frac{1.5}{T/2} = 0.2$$

Velger α i reg. systemet

~~at~~ være dobbel så nær som prosessen

$$K_p = \frac{2 \cdot 0.6 \cdot 0.2 \cdot 15 \cdot 1}{0.2} = 13$$

$$T_i = \frac{2 \cdot 0.6 \cdot 0.2 \cdot 15 \cdot 1}{0.2^2 \cdot 15} = 4.33$$

2) Pol/multiplet kansellering

$$T_M = \frac{T}{2} \quad K_p = \frac{T}{T_M K} = \frac{15}{7.5 \cdot 0.2} = 10$$

$$T_i = T = 15$$

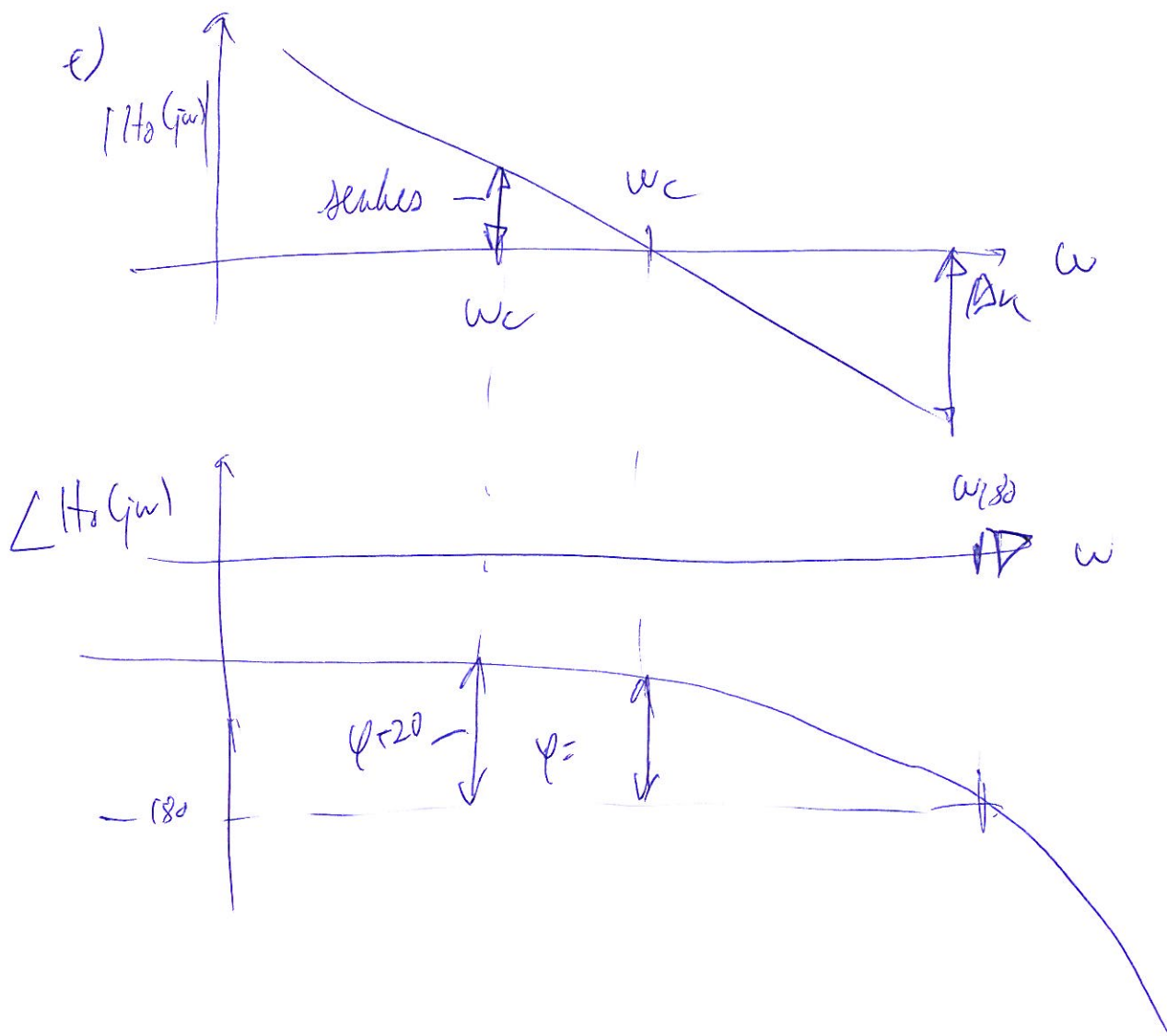
d) Når prosessen har dødtid, må reg. para være slakkere. Dette ser vi faktisk er tilfelle i b) og c). Grunnen til at reg. para må være slakkere er at dødtiden gjør at stabilitetsmarginene blir dårligere (11)

$$e) \quad H_p(s) = \frac{0.2}{15s+1} e^{-2s}$$

$$\begin{aligned} H_r(s) &= \frac{K_p T_i s + K_p}{T_i s} = \frac{33.75 \times 6.6 s + 33.75}{6.6 s} \\ &= \frac{222.75 s + 33.75}{6.6 s} \end{aligned}$$

$$H_o(s) = H_m(s) H_p(s) - H_r(s)$$

$$= 1 \cdot \frac{0.2}{15s+1} e^{-2s} - \frac{222.75 s + 33.75}{6.6 s}$$



- f) For å øke fasemargin, ser du etter den nye fellesaksen ω_c som gir $\varphi + 20$. For å få ω_c til å flytte seg mot venstre, må du senke $|H_0(j\omega)|$ så mye som indikert over. Hvis denne er f.eks. 10 dB, må du redusere K_p med 10 dB, dvs $\frac{K_p}{10 \text{ dB}} = \frac{K_p}{3.16} = K_{p,ny}$

Økt fasemargin \Rightarrow ~~økte~~ mindre oversving i sprangresponsen